<u>Checking Report</u> <u>for</u> <u>Wi Column</u> <u>by</u> <u>Wembley Innovation Limited</u>

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Issue date:	02/07/2015
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Comparison of Lateral Supports: Ancon WP2 Windpost vs Wi Beam

Introduction

This study compares a stainless steel $130 \times 70 \times 6$ WP2 Ancon windpost against a Wi Beam. For this case, the windpost and Wi Beam are required to support a 140mm blockwork wall 9m long and 4m high, subjected to a lateral pressure of 1.0kPa.

Panel Design



Windpost sub-panel capacity calculation

Refer to CADS wall panel calculation sheet W140/MaxL/01:

For a 140mm wall, 4m height and load pressure = 1.0kPa, the maximum sub-panel length = **2750mm**

Windpost calculation

From Table 1, which is based on Ancon windpost load capacities, select 130 x 70 x 6 WP2 section, which is the largest capacity windpost suitable for a 140mm wall.

For a 140mm wall, 4m height and load pressure = 1.0kPa, the maximum allowable panel length = **1860mm** (i.e. maximum windpost spacing)

Therefore, if the wall is restrained by the primary structure at either end and along the head, the number of panels formed are: 9,000/1860 = 5no. with 4no. windposts, spaced at 1800mm centres, as below:



Ancon WP2 windpost and panel layout

Wi Beam calculation

Refer to Wi Design Program page WiB/01:

For 140mm wall, 4m height, load pressure = 1.0kPa, if the wall is split into three sub-panels vertically (1183mm high), the Wi Beam is satisfactory, with a **Utilisation Ratio = 0.71**.

Wi Beam sub-panel capacity calculation

Refer to CADS wall panel calculation sheet WiB/W1:

For a 140mm sub-panel, 1.183m in height and 9.0m in length, subject to a load pressure = 1.0kPa, the sub-panel is satisfactory with a **utilisation ratio of 0.435**.

Therefore, the Wi Beam and sub-panel layout is:



Wi Beam and panel layout

Conclusions

- 1. For the same conditions, 4no. 130 x 70 x 6 WP2 Ancon windposts are required versus 2no. Wi Beams.
- 2. The 4no. Ancon WP2 windposts are at maximum capacity, whilst the 2no. Wi Columns are at a utilisation of only 71%.
- 3. The adopted Ancon WP2 windpost capacity is based on creating a fully mortared joint against the blockwork panels on both sides of the windpost. If a movement joint is required, the capacity will be **reduced**.
- 4. The comparison is for a standard 140mm Wi Beam and the highest capacity Ancon WP2 windpost that can be accommodated within a 140mm blockwork wall.
- 5. Note that there are 4no. vertical joints at the Ancon WP2 windpost positions. No joints are required for the Wi Beam option
- 6. The provision of the Wi Beams, which incorporate vertical shear transfer rods, eliminates the need for any shrinkage crack-control bedjoint reinforcement within the sub-panels

WEMBLEY INNOVATION [™]	SUSTAINABILITY CHECK	Job No	:
	Wi Beam vs Windpost Check	Job Ref	:
		Designed By	: TS
	Maximum Panel Length Calculation	Checked By	:
		Date	: 09/07/15
	140mm Wall 4000 high x 2750 long	Revision No	:
	Wind load = 1.0kPa	Calc No	: W140/MaxL/01
		Page No	: 1

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		-		>				Data ite	em	Near
Lateral supr	oorto		<u>//(0.00)////</u>				Bed	joint reinf	orcement	No
Lateral supp	JUILS						DPC	; - top		No
required to							DPC	- bottom		No
edges of panel						Note 1.Fo joint cour desig 2.Fo 'Deta 3.Fig show defir fixity befo	Note: 1.For details of masonry units joint reinforcement and damp course refer to 'Material and design data' 2.For details of wall ties (if specified) refer to 'Concise' o 'Detailed' report. 3.Figures in brackets eg: (1.C shown in elevation indicate u defined proportional fixity/continuity factor applied before allowing for openings.			
Maganny abarastaria	tio otror	atho								
Masonry characteris	suc strer		~	Unito	Desorin	tion		Near		Linita
Design and			(/ 006 1 1.0	Units	Descrip	lion		ivear		Units
Comprossion			990-1-1.2	005	Shear without a	omercoolon		0.15		NI/mm2
Compression	nt	1.0	`		Shear without of	compression		0.15		N/mm²
Factor for collar join	nt 	1.00	0 -		Snear inclion	coefficient		0.40		- N1/ma ma 2
Compression on be	ed joints	5.7	5	N/mm²	Limiting shear	bondod		0.65		N/mm²
Compression // bec	a joints	5.73	3	N/mm²		Donaea				N/mm²
Flexure	ire		_		Elastic modulus			F 70		
Horizontal span	Horizontal span 0.53		3	N/mm ²	Short term			5.73		kN/mm ²
Vertical span 0.22 N/mm ²				Long term			2.29		kN/mm ²	
Characteristic vertic	al loads				Characteristic lat	teral wind p	essure	0"	NI-4	Decision
Load category name		Ne	ar		Category name	Dyn. pr. kN/m²	Coeff.	Coeff.	Net	Kes. pr.
	Loa	ad (kN/m)	Eco	. mm	Wind near	1.000	0.700	-0.300	1.000	1.000
					Characteristic lat	teral line loa	d			
					Category name	Load k	N/m	Heigh	nt from bo	ottom mm
					Note: For details of	f more than	two loade	nlease ro	for datail	ad report
Summary results (or	itical los	ad combinatio	ns)			n more undit	10000	picase le	nor uciali	
Description		Wall	Statu	s Inits	Descripti	ion	Near		St	atus Elnits
Lateral load capacity	,	1 6	10	kN/m ²	Max slenderness	s ratio	, tou		27	
Design uniform load		kN/m ²	Actual		g	2.821				
Utilisation 0.932 Pass			Utilisation			C	.364 Pa	ss		
Load combination 0.90D+1.50Wn						Ŭ				
Limiting dimension /	area									
Allowable			90	mm						
Actual		1	40	mm						
Utilisation		0.6	43 Pass							
	I	0.0		I	1					

Notes:

• This is an example calculation to determine the maximum panel length for a 140mm block wall 4m in height and 9m in overall length, subject to a wind load of 1.0kPa

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• The maximum panel length is 2750 and will require structural supports to its edges if it is an internal panel to a continuous wall

Comparison of Ancon WP2 Windpost vs Wi Beam

TABLE 1

Note: Values will be based on full restraint of long leg of angle i.e. no provision of movement joint. If MJ is required, values are likely to be considerably reduced

Design spacings of WP2 windposts

	Max Total Design UDL (kN) per Post (from Ancon Tables)									
130x70x6	15.83	11.93	9.3	7.42	6.03	4.98	4.17	3.53		
		Height (m)								
Wind kPa	2.50	3.00	3.50	4.00	4.50	5.00	5.50	6.00		
0.25	25.33	15.91	10.63	7.42	5.36	3.98	3.03	2.35		
0.50	12.66	7.95	5.31	3.71	2.68	1.99	1.52	1.18		
0.75	8.44	5.30	3.54	2.47	1.79	1.33	1.01	0.78		
1.00	6.33	3.98	2.66	1.86	1.34	1.00	0.76	0.59		
1.25	5.07	3.18	2.13	1.48	1.07	0.80	0.61	0.47		
1.50	4.22	2.65	1.77	1.24	0.89	0.66	0.51	0.39		
1.75	3.62	2.27	1.52	1.06	0.77	0.57	0.43	0.34		
2.00	3.17	1.99	1.33	0.93	0.67	0.50	0.38	0.29		
2.25	2.81	1.77	1.18	0.82	0.60	0.44	0.34	0.26		
2.50	2.53	1.59	1.06	0.74	0.54	0.40	0.30	0.24		
2.75	2.30	1.45	0.97	0.67	0.49	0.36	0.28	0.21		
3.00	2.11	1.33	0.89	0.62	0.45	0.33	0.25	0.20		

Figure in red used to compare against Wi Beam design

Figures in grey are uneconomic / impractical spacings

Wambley Innevation 1 td			
38A Fourth Way, Wembley, Middlesex, HA9 0LH	Ancon WP2 vs Wi Beam	Job No:	
office@wembleyinnovation.co.uk		Revision	
Tel: 0208 903 4527	Prepared By: TS	Page: WiB/01	
Wall Ref.: Comparison with Ancon 130x70x6 WP2	Checked By:	Date: 09/07/2015	
GENERAL DATA	SUMMARY OF R	ESULIS	
Element type: Wi Beam	Wi Beam	utilisation ratio = 0.71	
Design approach: Standard	ADOPT: 140mm thk We	mbley Innovation Wi Beam	
ELEMENT ARRANGEMENT	DESIGNER'S N	OTES	
Wi Beam height: Single	Use Wi Beams to span 11m long pan	el	
Upper section construction type: Standard	4m high Panel is split into 3, giving su	ub-panels = 1.183m high	
Lower section construction type: Standard			
Wall thickness 't' [mm] = 140			
Panel length 'L' [<i>m</i>] = 9.00			
Distance to top support's face $w_1'[m] = 1.18$			
Distance to bottom support's face 'w ₂ ' [<i>m</i>] = 1.18	Colour coding not required colour coding		
UNFACTORED LOADING	CALCULATIO	INS	
Lateral wind load $W_k' [kN/m^2] = 1.00$	Unfactored reaction left /	right 'R' <i>[kN] = 5</i> .97 / 5.97	
Barrier distributed load $W_{b UDL} [kN/m^2] = 0.00$	Unfactored moment: v	vind load [kNm] = 14.16	
Barrier line load 'W _{b_line} ' [kN/m] = 0.00	Unfactored moment: barrier di	stributed [kNm] = 0.00	
Barrier height 'h _b ' [m] = 0.00	Unfactored moment: barrier	line load [kNm] = 0.00	
Partial load factor for wind load $\gamma_{f} = 1.50$	Total applied factored mom	ent 'M _{Ed} ' <i>[kNm]</i> = 21.24	
Partial load factor for barrier load ' γ_{f} ' = 1.50	Moment of resista	nce 'M _{Rd} ' <i>[kNm]</i> = 30.00	
Partial material factor $\gamma_{M}' = 2.00$ (?)	ADOPT: 140mm thk W	embley Innovation Wi Beam	



NOTES:

1. Clear span between columns is edge-to-edge of columns (not centre-to-centre);

2. Panel is assessed as having simple support conditions to all 4 sides;

3. Classic "back of envelope" failure of the panel is assumed to occur with 45° yield lines at corners;

4. Sub-panels to be designed according to BS EN1996-1.1.

WEMBLEY INNOVATION™	SUSTAINABILITY CHECK	Job No	:
	Wi Beam vs Windpost Check	Job Ref	:
		Designed By	: TS
	Panel Check Calculation	Checked By	:
		Date	: 09/07/15
	140mm Wall 1183 high x 9000 long	Revision No	:
	Wind load = 1.0kPa	Calc No	: WiB/W1
		Page No	: 1

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Notes:

 This is an example calculation to check sub-panels of a 140mm block wall 4m in height and 9m in overall length, subject to a wind load of 1.0kPa

• For 2no. Wi Beams, the 3no. sub-panels are 1183mm high